

Sustainability Assessment of LC³-based Reinforced Concrete in Simulated Corrosive Semi-arid Environment of Morocco

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Abstract

This study investigates the sustainability performance of local common raw clay as a supplementary cementitious material (SCM) in concrete in simulated semi-arid environment of Morocco. The service life of the underground concrete pipe is shorter in this harsh environment because of aggressive corrosive soil, and cyclical variation of temperature and humidity. Limestone cement calcined clay (LC³) and limestone cement fly ash (LCF) and traditional OPC (Ordinary Portland cement) have been investigated. The electrochemical resistance, environmental, and economical performances have been evaluated. In the simulated condition, the LC³ improve good concrete performance (R_c) in simulated condition by approximately 25 and 3 times compared to LCF and OPC, respectively. The environmental and economical assessments of LC³ and LCF binder showed a similar cost and embodied CO₂, and both concrete mixes were lower by 38% and 38%, respectively, than the traditional concrete. Ultimately, the LC³ technology seems to improve eco-friendly sustainability performance in the simulated aggressive semi-arid environment.

Keywords

Calcined clay, Limestone cement calcined clay, Fly ash, Sustainability, Corrosion, Aggressive soil, Wetting drying cycles, Chloride, Sulfate

Introduction

Cement fabrication contributes about 7% to the global CO₂ footprint [1]. However, the demand for building material is advancing due to the rapid development in the construction sector. Blended cement with SCMs which replace a part of clinker is the most interesting solution nowadays. The most SCMs materials used in Morocco are Silica fume and fly ash [2, 3] although these industrial products have a production limitation of only 15% global availability [4]. It is stated in previous research that calcined clay as SCMs improves the durability and sustainability of concrete blends [5, 6]. A study in Cuba shows that LC³ allows sustainability increase by reducing the climate and social impacts per cost [7], as well as carbon emission, and energy consumption [8]. Also, a recent study in Brazil opened a new perspective for the production of alternative low-carbon and eco-friendly LC³ cement [9].

In this paper, the sustainability performance of the calcined clay and fly ash was evaluated by comparing the LC³ and LCF blend to the traditional concrete.

The aim of this study is to evaluate the environmental impact and economic potential of LC³ and LCF compared to the OPC in simulated harsh environment of aggressive corrosive soil, and cyclical variation of temperature and humidity.

Our findings may encourage both the researchers and industrials in Morocco and in other counties to use calcined clay as SCMs.

Experimentation

Materials proprieties

Portland cement CEM I, limestone and clinker were sourced locally LafargeHolcim Morocco. A common clay was calcined in a laboratory oven at 800 °C for 1 h to achieve high pozzolanic reactivity [10, 11], and fly ash class F obtained from Jorf Lasfer power Morocco were used as SCMs. LC³-based concrete are nanoscale materials. The chemical compositions of the materials are listed in table 1. The scanning electron microscope images of fly ash and calcined clay particles are shown in figure 1.

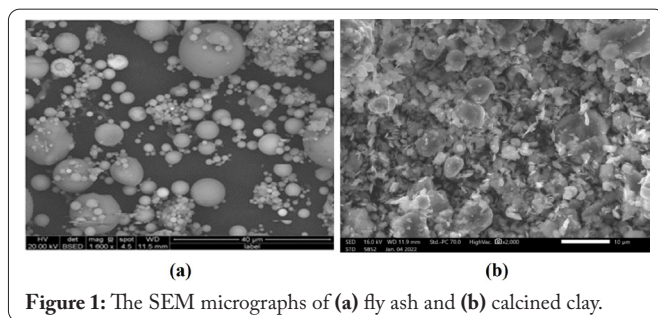


Figure 1: The SEM micrographs of (a) fly ash and (b) calcined clay.

Table 1: Chemical composition of clinker, calcined clay, fly ash, and limestone (wt.%).

	Clinker	OPC	Fly ash	Calcined clay	Limestone
SiO ₂	20.69	15.18	39.5	37.06	8.37
Al ₂ O ₃	5.60	3.68	33.4	10.38	1.87
CaO	64.98	58.42	8.36	23.62	45.83
Fe ₂ O ₃	3.67	2.36	3.35	3.99	0.83
K ₂ O	0.83	0.56	0.81	1.64	0.13
MgO	2.51	2.55	2.06	2.88	3.56
Na ₂ O	-	0.09	1.13	-	0.04
SO ₃	1.34	2.59	0.4	0.37	0.09
Cl	-	0.01	-	-	-
Na ₂ O _{eq}	-	0.45	-	-	-
CaO _{free}	0.38	-	-	-	-
LOI	-	14.58	8.5	20.06	39.28

Mix proportions and test specimen preparation

The calcined clay was mixed with limestone, and clinker to prepare the LC³ binder. As well fly ash was mixed with limestone and clinker to prepare LCF mix. The OPC was used as control. In order to have a good correlation and to compare the results, the two binders were prepared with same mass ratio of calcined clay (fly ash): limestone in LC³ (LCF) mixtures of approximately 1:1. The mix compositions are listed in table 2. All the specimens were unmoulded after 24 h and left to cure at 24 ± 1 °C and 100% relative humidity for 28 days.

Environmental test

In this study soil with a concentration of 9 g chloride and 34 g/kg sulfate was used to simulate the environmental

Table 2: Concrete mix composition of the mixes.

	OPC	LC ³	LCF
CEM1 (kg/m ³)	450	0	0
Clinker (kg/m ³)	0	280	280
Calcined clay (kg/m ³)	0	76	0
Fly ash (kg/m ³)	0	0	76
Limestone (kg/m ³)	0	94	94
Aggregate (kg/m ³)	1284	1284	1284
Sand dune (kg/m ³)	536	536	536
Water (L/m ³)	172	172	172
W/B	0.38	0.38	0.38

conditions of semi-arid area in Morocco. Specimens prepared from different mixes OPC, LC³, and LCF were buried in this aggressive soil and exposed to 16 wetting and drying cycles as indicated in the previous study. The dry cycle takes 5 days in a laboratory oven at 60 °C, and the wet cycle takes 2 days under water saturation at ambient temperature, which set 7 days of each cycle [12].

Electrochemical measurements

The electrochemical concrete/reinforcement resistances against the chloride-sulfate penetration were measured by using three electrodes electrochemical cell Potentiostat (PGZ100) (Figure 2) following the methodology in the reference [6]. The measurements were performed at different wetting drying cycles under 10 mV alternating current signal from an initial frequency of 100 MHz to a final frequency of 10 mHz [13].

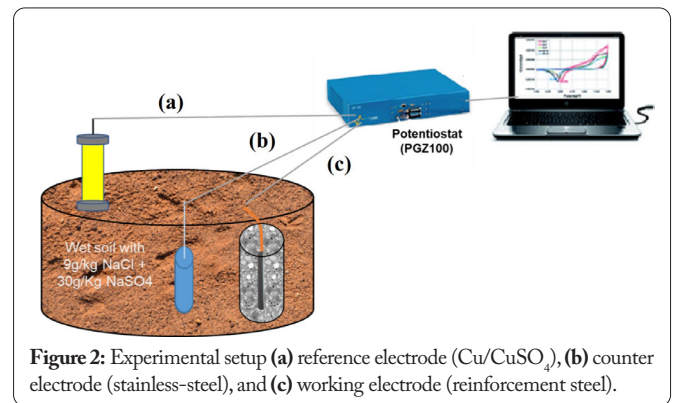


Figure 2: Experimental setup (a) reference electrode (Cu/CuSO₄), (b) counter electrode (stainless-steel), and (c) working electrode (reinforcement steel).

Results and Discussion

Electrochemical results

Figure 3 shows the ion transfer resistance R_c of the concrete mixes OPC, LCF, and LC³ as a function of cyclic wetting drying got from electrochemical data modelling results. it can be seen that the electrochemical parameter R_c of the LCF blended cement is higher than the reference OPC, while LC³ shows the highest value by approximately 3 times compared to the LCF. This indicates clearly that the concrete incorporated calcined clay can be limit the chloride-sulfate ion transport process in the LC³ binder [14, 15]. Furthermore, the resistance evolution of LC³ improves throughout the cyclic variation,

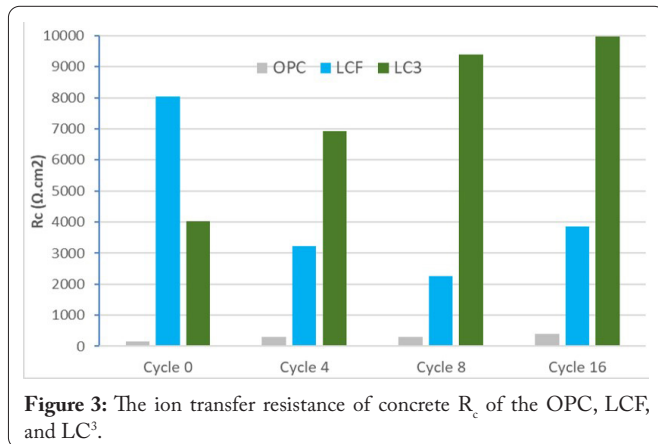


Figure 3: The ion transfer resistance of concrete R_c of the OPC, LCF, and LC³.

while both OPC and LCF decrease as the wetting-drying cycles progress. the excellent resistance of LC³ concrete against chloride ingress can be attributed to the pozzolanic reaction of amorphous aluminosilicate (Al₂Si₂O₇) product of the calcined clay with calcium hydroxide to form more silicate (CSAH) and alumina hydrate that fill the pore structure, outcoming to a denser structure matrix [16]. On other hand, the alumina of calcined clay reacts with the calcium carbonate of limestone to give hydrates product of carbo-aluminate (C₃ACcH) [6, 17].

Environmental evaluation of embodied carbon and material cost

In this study as all the mixes have the same proportion and composition formulation, the comparison of environmental and economic impacts focuses only on the binder effect, not including other ingredients (gravel, sand, and water). Emission factors Kilogram of CO₂ emitted per Kilogram of material produced was considered in the estimate of mitigation potential [18]. The average cost of LC³ and OPC was estimated based on the average local market price in Morocco. The cost and CO₂ emission of different materials are listed in table 3. Based on equation (1) the results are presented in figure 4. In addition, the resistance of concrete R_c, was considered for the evaluation of the sustainability performance of each mix. The parameters of traditional OPC binders are considered as the reference. It can be seen in figure 4a that the total embodied carbon of LC³ and LCF was approximately similar although the fly ash incorporated in LCF mix is considered negligible, and both were lower than OPC by approximately 32% and 38% respectively. Figure 4b presents the material cost of the three concrete mixes. Both LC³ and LCF binders showed the same cost by contributing to about 67% of the total material cost for traditional concrete.

To determine a relationship between these parameters and the environmental/economic impact, the indices below

Table 3: Cost and CO₂ emission of ingredient (the average cost is estimated based of the local market price).

	CO ₂ emission (kg/t)	Average market cost (USD/t)
OPC	912 [19]	125
Fly ash	8 [19]	20
Calcined clay	330 [20]	18
Limestone	10	15

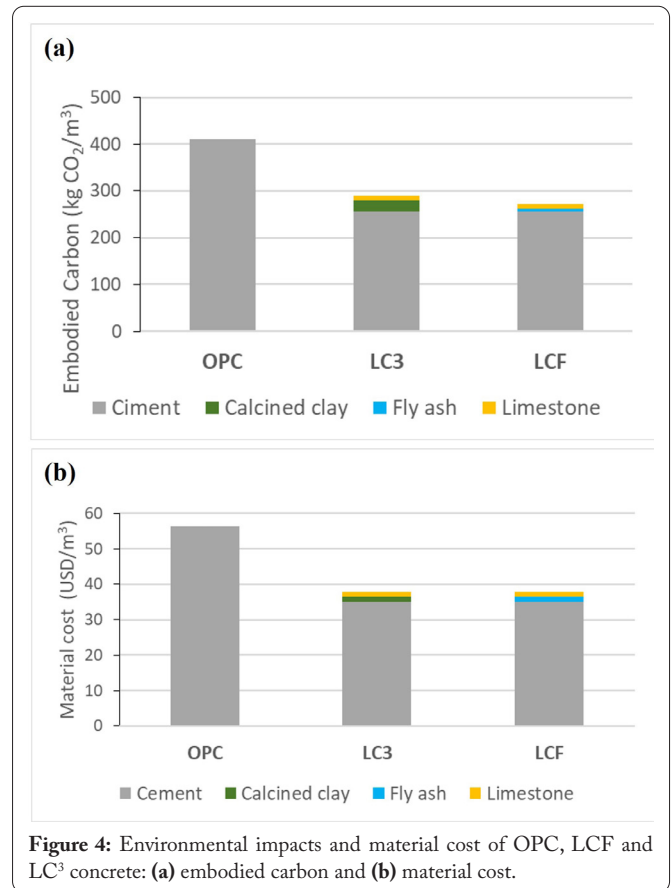


Figure 4: Environmental impacts and material cost of OPC, LCF and LC³ concrete: (a) embodied carbon and (b) material cost.

are calculated [19]:

$$R_c |Cost| embodied CO_2 Index = \frac{Value\ for\ OPC}{Value\ for\ LC^3\ |LCF} \quad (1)$$

$$Global\ Performance\ Index = \frac{\sum_{i=3} Indices\ for\ LC^3\ |LCF}{\sum_{i=3} Indices\ for\ OPC} \quad (2)$$

A trade-off between the electrochemical resistance, and environmental/economic potential was considered to evaluate the sustainability of the OPC, LCF, and LC³ binders. The sustainability performance of the three concrete mixes is quantified based on the equations (1 and 2) in the graph presented in figure 5. The higher the index value the higher performance. It is interesting to note that the LC³ mark a higher global performance index by 2 times more than LCF

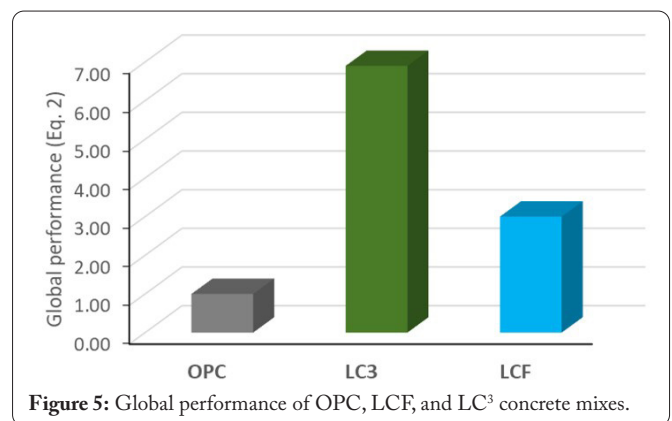


Figure 5: Global performance of OPC, LCF, and LC³ concrete mixes.

mix, and approximately 7 times compared to the traditional OPC concrete.

Conclusions

In this study, the electrochemical resistance, environmental, and economical performances of OPC, LCF, and LC³ concrete mixes were investigated. The three binders were tested in a simulated environment of semi-arid area under wetting-drying cycles. According to the experimental measurement, the following main results could be drawn:

- The resistance R_c of LC³ was higher than LCF and OPC control.
- The total embodied carbon of LC³ and LCF was approximately similar, and both were lower than OPC by approximately 32% and 38%, respectively.
- The LC³ and LCF binder showed the same cost by contributing about 67% of the total material cost for traditional concrete.
- The sustainability of LC³ compared to the OPC was approved by the higher global performance index, which is 2 times more than LCF mix, and approximately 7 times compared to the traditional OPC concrete.

Ultimately, the LC³ technology seems to improve eco-friendly sustainability performance in the simulated aggressive semi-arid environment.

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Conflict of Interest

None.

References

- Shanks W, Dunant CF, Drewniok MP, Lupton RC, Serrenho A, et al. 2019. How much cement can we do without? Lessons from cement material flows in the UK. *Resour Conserv Recycl* 141: 441-454. <https://doi.org/10.1016/j.resconrec.2018.11.002>
- Ech-chebab A, Ejbouh A, Galai M, Hassi S, Berrami K, et al. 2021. Assessing the fly ash effect on the durability of reinforced concrete of water treatment tanks exposed to coagulating ferric chloride by an electrochemical process. *J Bio Tribo Corros* 7: 1-17. <https://doi.org/10.1007/s40735-021-00513-8>
- Ech-chebab A, Ejbouh A, Galai M, Hassi S, Belhaj T, et al. 2022. The individual and combined effect of olive stone biomass ash with coal fly ash on the durability of water treatment tank concrete exposed to ferric chloride. *Chem Africa* 5(6): 2067-2084. <https://doi.org/10.1007/s42250-022-00458-6>
- Scrivener KL. 2014. Options for the future of cement. *Indian Concr J* 88(7): 11-21.
- Ejbouh A, Ech-chebab A, Galai M, Hassi S, Benqlilou H, et al. 2022. Calcined clay process for durability performance of concrete pipe in simulated semi-arid area in Morocco. *Mater Today Proc* 58: 1403-1407. <https://doi.org/10.1016/j.matpr.2022.02.332>
- Ejbouh A, Ech-chebab A, Hassi S, Galai M, Benqlilou H, et al. 2023. Durability assessment of LC³-based reinforced concrete under combined chloride-sulfate environment via the EIS technique. *Constr Build Mater* 366: 130194. <https://doi.org/10.1016/j.conbuildmat.2022.130194>
- Berriel SS, Ruiz Y, Sánchez IR, Martirena JF, Rosa E, et al. 2018. Introducing Low Carbon Cement in Cuba-A Life Cycle Sustainability Assessment Study. In Martirena F, Favier A, Scrivener K (eds) *Calcined Clays for Sustainable Concrete*. Springer, Dordrecht, pp 415-421.
- Sánchez S, Cancio Y, Sánchez IR, Martirena JF, Rosa ER, et al. 2019. Sustainability assessment in Cuban cement sector-a methodological approach. *IOP Conf Ser Earth Environ Sci* 323(1): 012128. <https://doi.org/10.1088/1755-1315/323/1/012128>
- Malacarne CS, da Silva MR, Danieli S, Maciel VG, Kirchheim AP. 2021. Environmental and technical assessment to support sustainable strategies for limestone calcined clay cement production in Brazil. *Constr Build Mater* 310: 125261. <https://doi.org/10.1016/j.conbuildmat.2021.125261>
- Du H, Dai Pang S. 2020. High-performance concrete incorporating calcined kaolin clay and limestone as cement substitute. *Constr Build Mater* 264: 120152. <https://doi.org/10.1016/j.conbuildmat.2020.120152>
- Filho SE, Panossian Z, de Almeida NL. 2013. A new copper/copper sulfate reference electrode for external corrosion monitoring of buried pipelines. In NACE CORROSION, Orlando, Florida, United States.
- Ejbouh A, Ech-chebab A, Galai M, Lachhab R, Benqlilou H, et al. 2022. Effects of fly ash and simulation of the natural hot and dry climate of the Moroccan desert region on the durability of prestressed concrete cylinder pipes. *J Pipeline Syst Eng Pract* 13(4): 04022029. [https://doi.org/10.1061/\(ASCE\)PS.1949-1204.0000658](https://doi.org/10.1061/(ASCE)PS.1949-1204.0000658)
- Berrami K, Ech-chebab A, Galai M, Ejbouh A, Hassi S, et al. 2021. Evaluation of fly ash effect on the durability of prestressed concrete cylindrical pipe in aggressive soil by electrochemical method. *Chem Data Collect* 32: 100656. <https://doi.org/10.1016/j.cdc.2021.100656>
- Nguyen QD, Khan MS, Castel A. 2020. Chloride diffusion in limestone flash calcined clay cement concrete. *ACI Mater J* 117(6), 165-175. <https://doi.org/10.14359/51725986>
- Shi Z, Ferreira S, Lothenbach B, Geiker MR, Kunther W, et al. 2019. Sulfate resistance of calcined clay-Limestone-Portland cements. *Cem Concr Res* 116: 238-251. <https://doi.org/10.1016/j.cemconres.2018.11.003>
- Scrivener K, Martirena F, Bishnoi S, Maity S. 2018. Calcined clay limestone cements (LC³). *Cem Concr Res* 114: 49-56. <https://doi.org/10.1016/j.cemconres.2017.08.017>
- Antoni M, Rossen J, Martirena F, Scrivener K. 2012. Cement substitution by a combination of metakaolin and limestone. *Cem Concr Res* 42(12): 1579-1589. <https://doi.org/10.1016/j.cemconres.2012.09.006>
- Environment UN, Scrivener KL, John VM, Gartner EM. 2018. Eco-efficient cements: potential economically viable solutions for a low-CO₂ cement-based materials industry. *Cem Concr Res* 114: 2-26. <https://doi.org/10.1016/j.cemconres.2018.03.015>
- Yu J, Mishra DK, Hu C, Leung CK, Shah SP. 2021. Mechanical, environmental and economic performance of sustainable Grade 45 concrete with ultrahigh-volume Limestone-Calcined Clay (LCC). *Resour Conserv Recycl* 175: 105846. <https://doi.org/10.1016/j.resconrec.2021.105846>
- Homayoonmehr R, Ramezaniyanpour AA, Mirdarsoltany M. 2021. Influence of metakaolin on fresh properties, mechanical properties and corrosion resistance of concrete and its sustainability issues: a review. *J Build Eng* 44: 103011. <https://doi.org/10.1016/j.job.2021.103011>